

Comparison of Green and Conventional Rocket Propellants: System Analysis Tool for in-space Propulsion

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Knowledge for Tomorrow

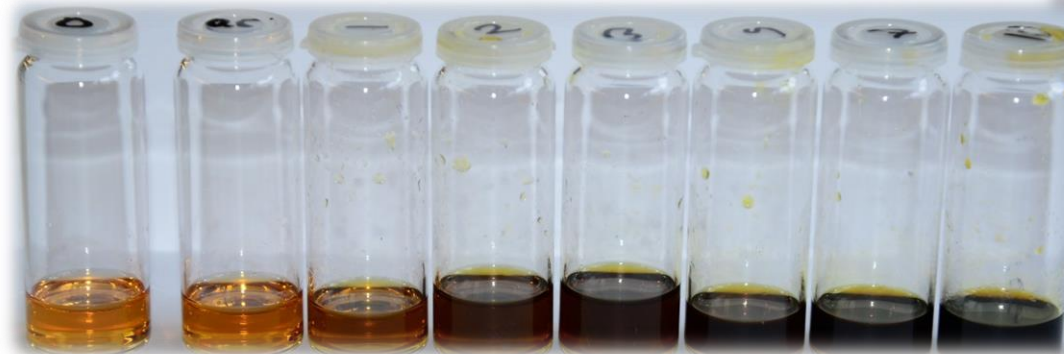
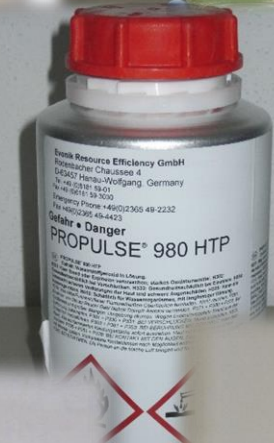
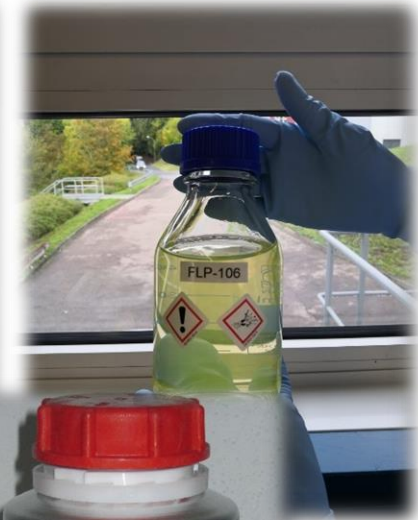
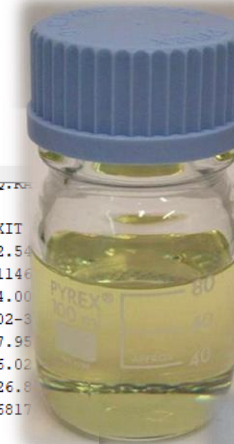


Motivation

Comparison of different propellants

- Global research activities on various green propellants
- Comparison often based solely on I_{sp}
- **But:**
 - Propellant density effects the performance of the overall system
 - Different propulsion system designs can offer additional advantages

07=-	1.63000	\$DEL=	37.735049	K, EQ=	3
	CHAMBER	THROAT	EXIT		
Pinf/P	1.0000	1.7506	872.54		
P, BAR	10.000	5.7124	0.01146		
T, K	3059.48	2859.15	764.00		
RHO, KG/CU M	8.0308-1	4.9549-1	3.7202-8		
H, KJ/KG	325.18	-346.10	-4437.95		
U, KJ/KG	-920.02	-1498.98	-4746.02		
G, KJ/KG	-38474.2	-36604.9	-14126.8		
S, KJ/(KG) (K)	12.6817	12.6817	12.6817		
M, (1/n)	20.429	20.620	20.620		
Cp, KJ/(KG) (K)	4.4693	3.7738	1.6462		
GAMMA	1.1554	1.1645	1.3244		
SON VEL, M/SEC	1199.5	1158.7	638.8		
MACH NUMBER	0.000	1.000	4.832		
PERFORMANCE PARAMETERS					
Ae/At		1.0000	50.000		
CSTAR, M/SEC		1741.8	1741.8		
CF		0.6652	1.7720		
Ivac, M/SEC		2153.7	3186.3		
Isp, M/SEC		1158.7	3086.5		
MOLE FRACTIONS					
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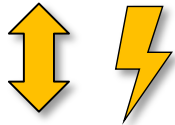


[2]

Motivation

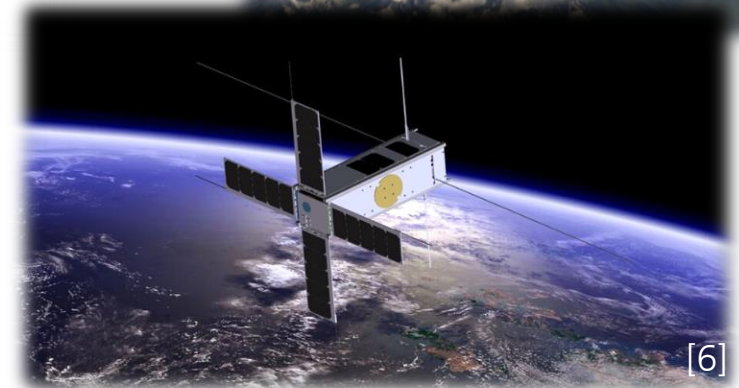
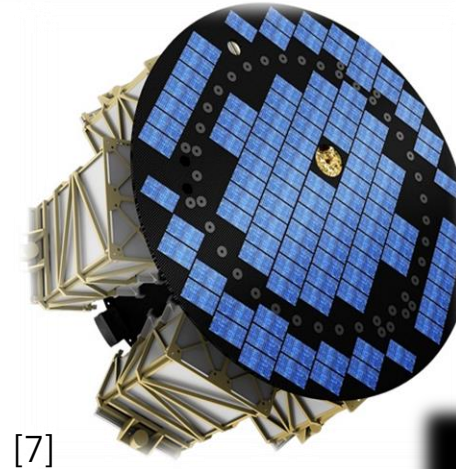
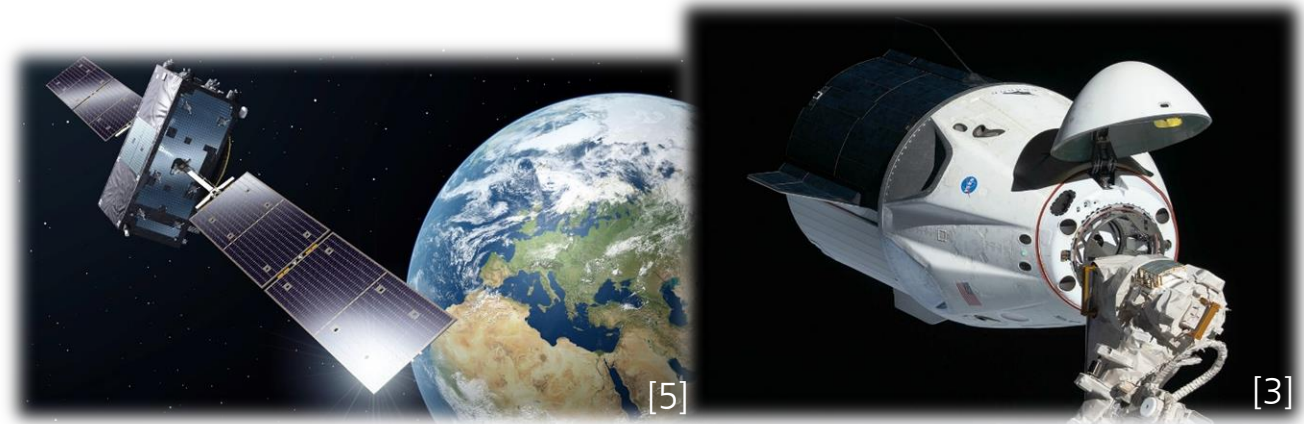
Comparison of different propellants

- “Best” propellant choice influenced by spacecraft size/mass and Δv budget
- Performance parameters of existing thrusters are known
- For lower TRL systems often only the theoretical performance is known

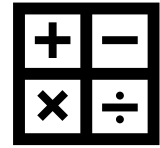


Aim:

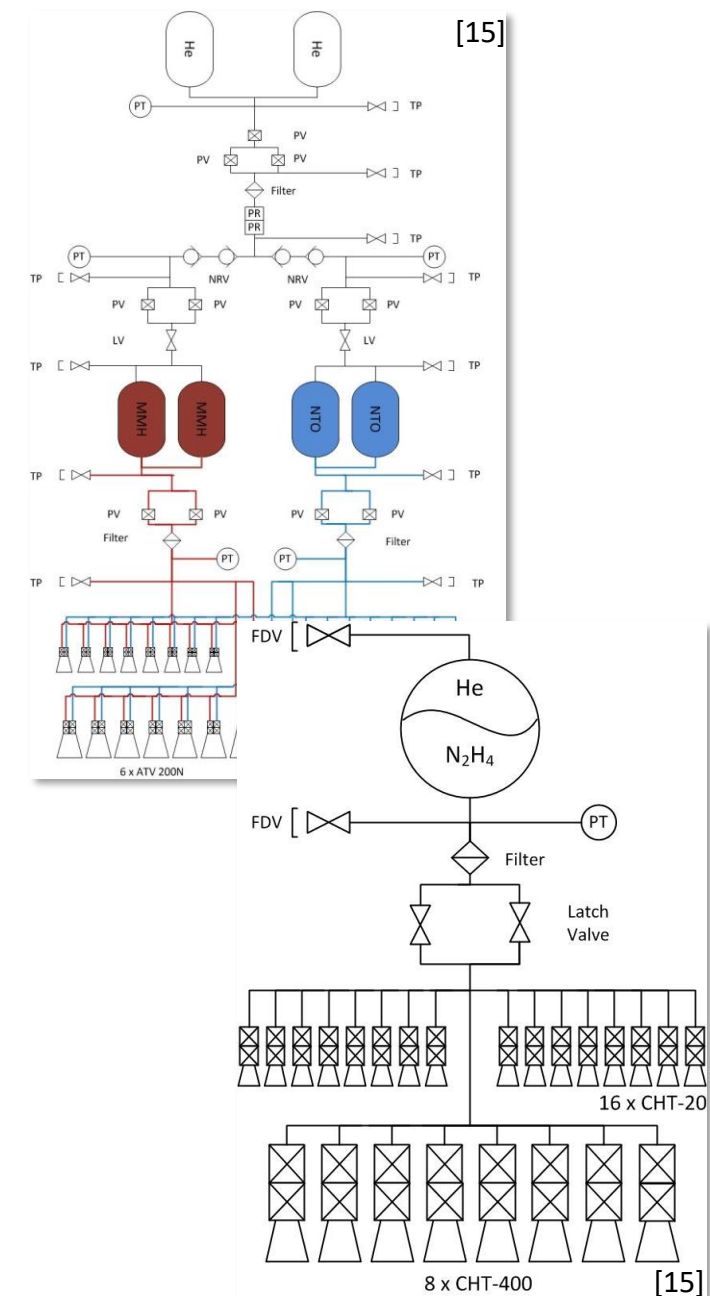
- Assess and compare the performance of different green propellants to conventional propellants on a system level
- Comparison of system mass and Δv



Background and assumptions



- Propellant and propulsion system data from literature [8-41], see reference list
- Performance based on experimental literature data, otherwise CEA calculations with adjustable efficiency losses
- Self-pressurization: No mass for pressurant tank, pressurant piping, pressurant valves and pressurant needed
- All tanks are spherical
- Calculation of tank thickness/mass with Barlow's formula depending on tank/propellant pressure
- Thruster masses based on existing mono- and bipropellant thrusters, system component's masses based on existing systems
- HyNOx thrusters have 50% more mass compared to non-HyNOx thrusters



Calculation steps

Spacecraft
Dry Mass

Mass without
propulsion
system

$$\Delta v = I_{sp} g_0 \ln \left(\frac{m_{sc\ dry} + m_{tanks} + m_{propellant} + m_{pressurant} + m_{prop\ sys}}{m_{sc\ dry} + m_{tanks} + m_{prop\ sys}} \right)$$

Volume of
propellant
tank

Selection of
propellant
and
efficiency

Number of
propellant
and
pressurant
tanks

Calculation
of Tank,
Pressurant
mass

Mass of propulsion
system without
tanks

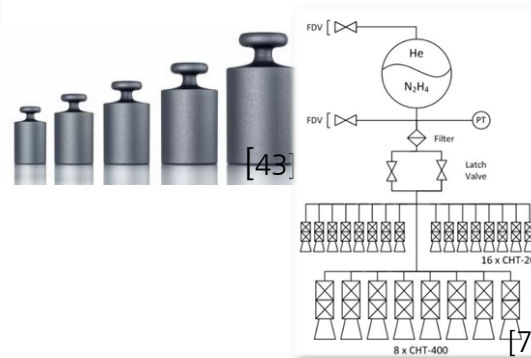
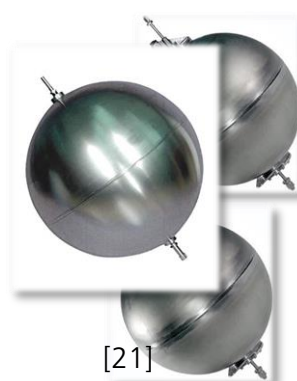
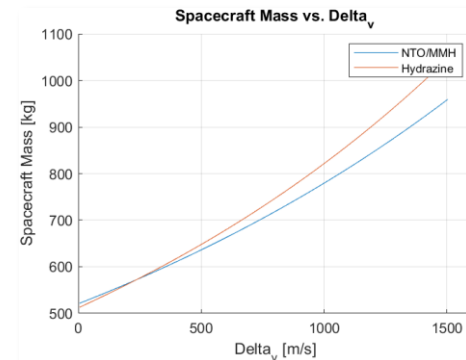
Calculation
of
propulsion
system dry
mass

For specific
conditions

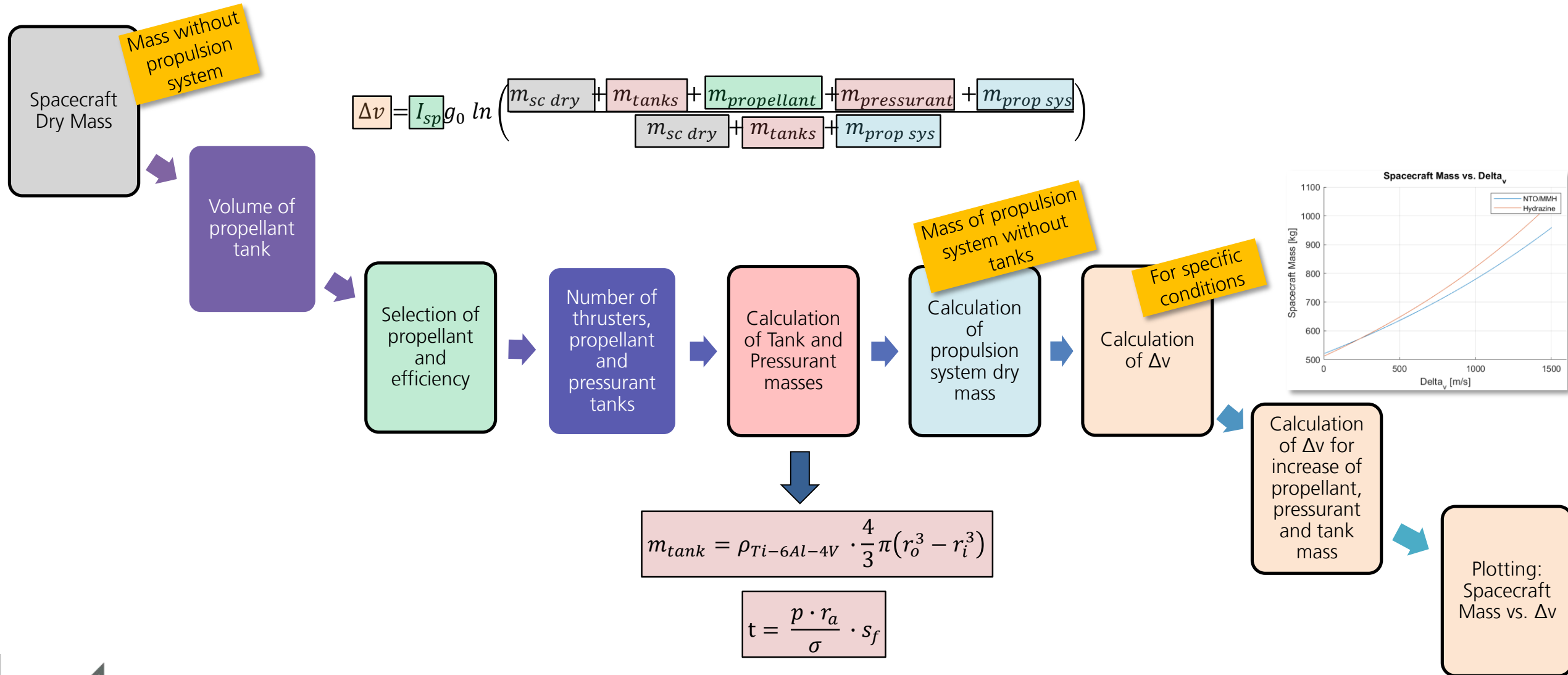
Calculation
of Δv

Calculation
of Δv for
increase of
propellant,
pressurant
and tank
mass

Plotting:
Spacecraft
Mass vs. Δv



Calculation steps

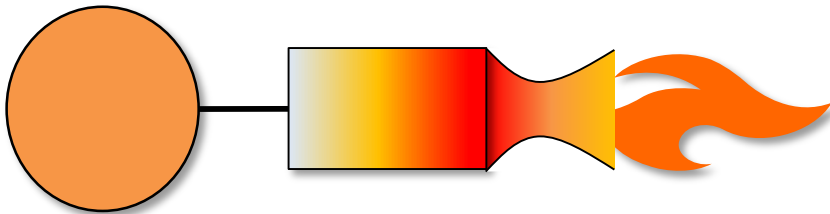


Propellants included

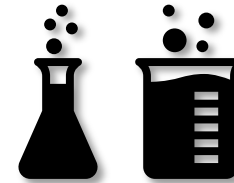
Monopropellants:



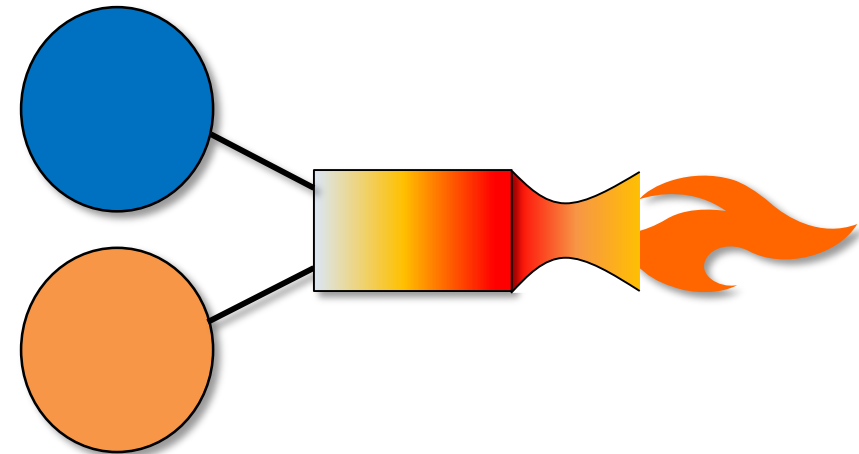
- N_2H_4
- LMP-103S
- FLP-106
- H_2O_2
- EUFB (European Fuel Blend, premixed $\text{N}_2\text{O}/\text{EtOH}$)
- HyNOx (DLR premixed $\text{N}_2\text{O}/\text{C}_2\text{H}_6$)
 - Self-pressurized
 - External pressurization
- AF-M315E
- SHP 163



Bipropellants:



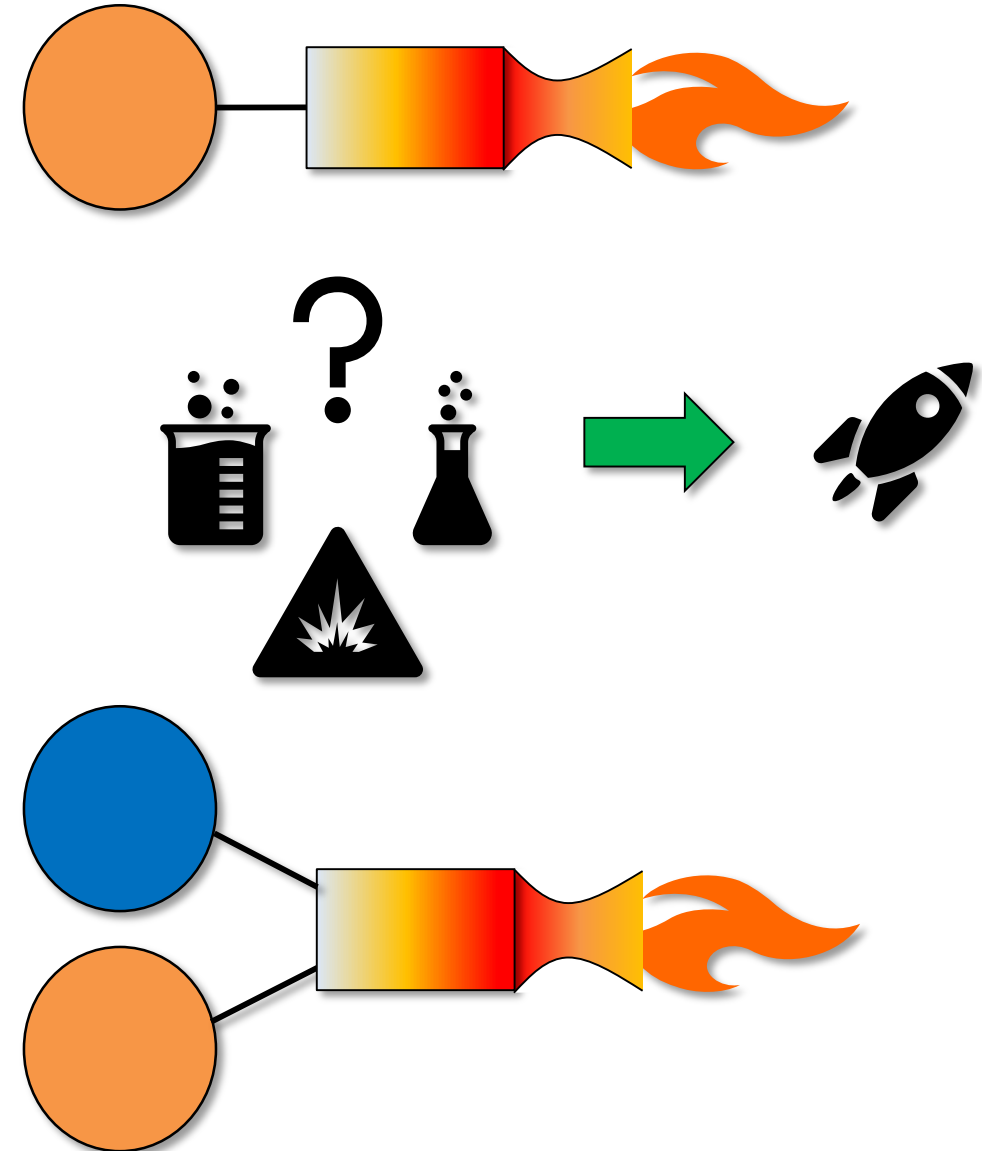
- MMH/NTO
- HIP_11 (DLR Hypergolic Bipropellant)
- HyNOx (DLR non-premixed $\text{N}_2\text{O}/\text{C}_2\text{H}_6$)
 - Self-pressurized
 - External pressurization



Propellants included

Generic propellants:

- Monopropellant, user input:
 - I_{sp}
 - Density
 - Self pressurized: Pressure inside the tank
- Bipropellant, user input:
 - I_{sp}
 - Oxidizer to fuel ratio
 - Density of oxidizer and fuel
 - Self pressurized: Pressure inside the tanks



User Interface:

Spacecraft Dry Mass

Propellant selection

Number of tanks

Propellant Tank Volume

Efficiency

Number of Thrusters

Results for the given conditions

Plot spacecraft mass vs. Δv

Comparison using Spacecraft Dry Mass and Tank Volume

Spacecraft Dry Mass [kg]
* This value does not include the propulsion system

Propellant Tank Volume [L]
* In the case of bipropellants, the volume is the sum of oxidizer and fuel

Existing Propellants Generic Propellant

Propellant 1
 Propellant 2

Efficiency [%]
 Efficiency [%]

Nr. Pressurant Tanks
* For non-self-pressurised propellants

Nr. Propellant Tanks
* In the case of bipropellants, this is the number of tanks for oxidizer and fuel

Nr. 22 N Thrusters
 Nr. 200 N Thrusters
 Nr. 400 N Thrusters

Calculate

Spacecraft Wet Mass 1 [kg] Delta_v Propellant 1 [m/s] Mass Propellant 1 [kg]
 Spacecraft Wet Mass 2 [kg] Delta_v Propellant 2 [m/s] Mass Propellant 2 [kg]

Spacecraft Mass vs. Δv

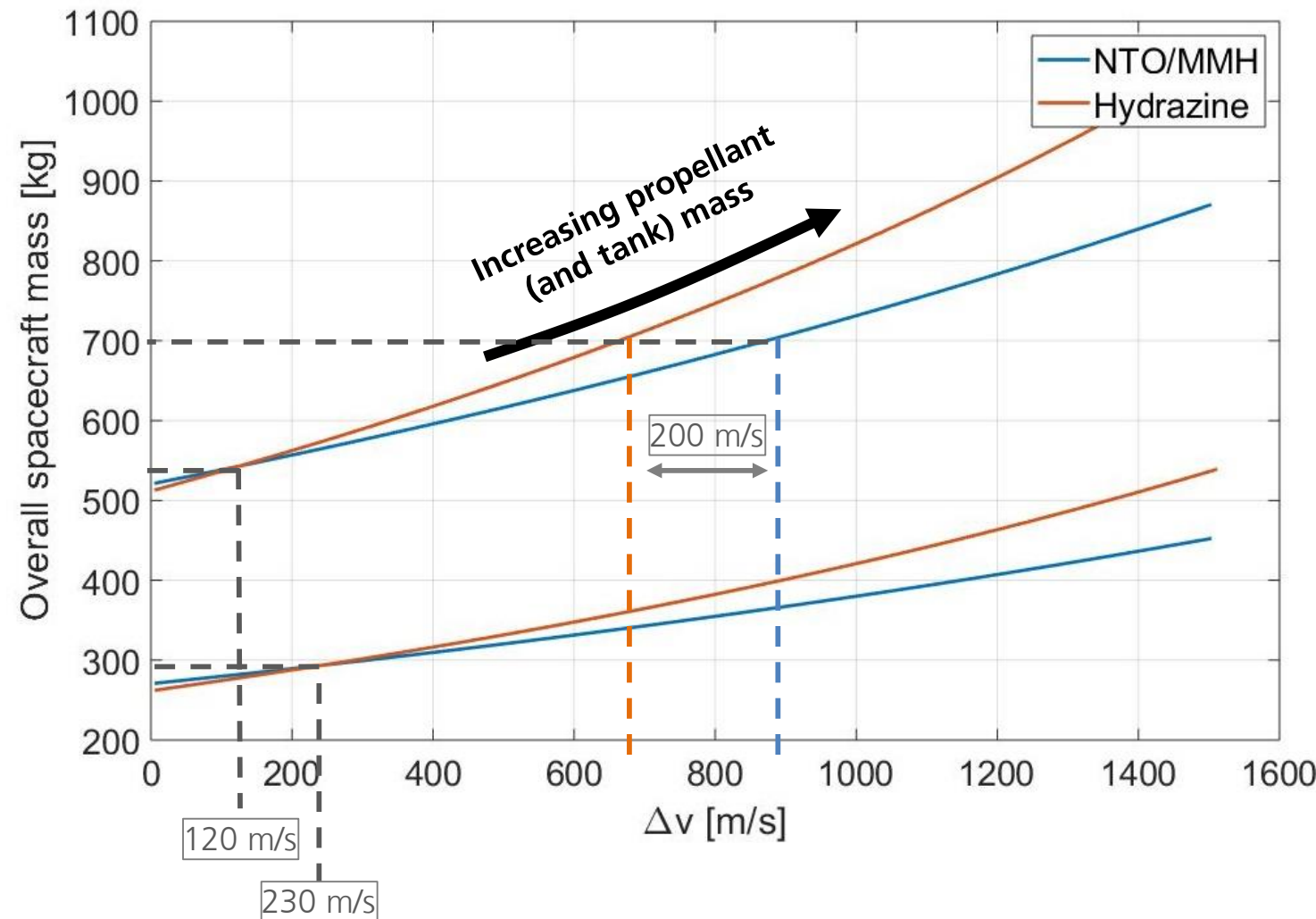
Back

Exemplary results

Hydrazine			NTO/MMH		
I_{sp}	ϵ	Eff. %	I_{sp}	ϵ	Eff. %
230	60	100	320	330	100

Comparison of mono- and bipropellant systems for 250 and 500 kg spacecraft dry mass

- For high Δv requirements the higher I_{sp} of bipropellant systems exceeds the drawbacks of higher system weights
- Pure monopropellant system results in lower spacecraft mass for
 - 250 kg spacecraft when up to 230 m/s Δv are needed
 - 500 kg spacecraft when up to 120 m/s Δv are needed
- For lower spacecraft masses, the lower masses of N_2H_4 systems are more advantageous



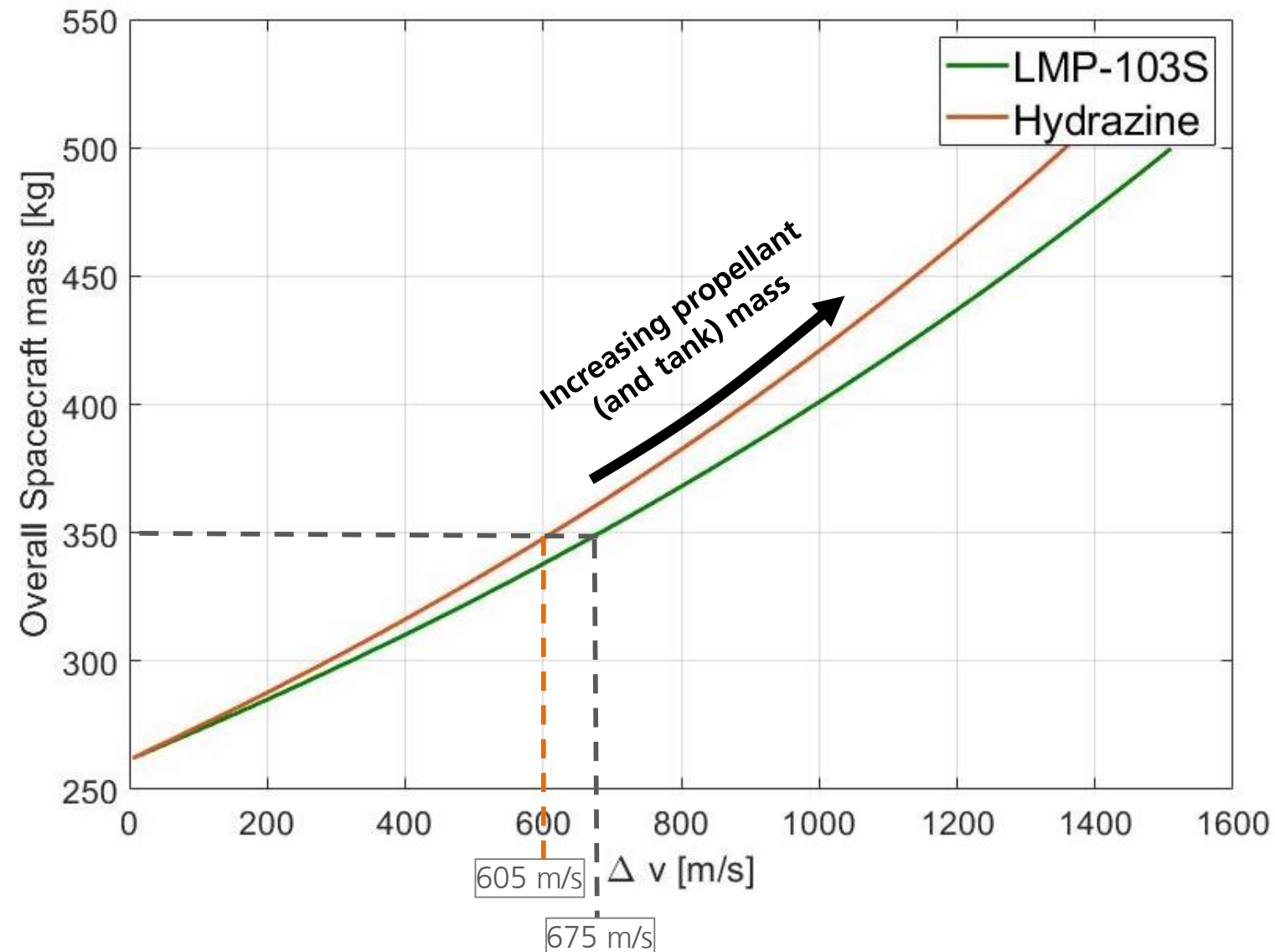
Exemplary results

Hydrazine		Eff.
I_{sp}	ϵ	%
230	60	100

LMP-103S		Eff.
I_{sp}	ϵ	%
253	150	100

Comparison of conventional and green mono- propellant systems for 250 kg spacecraft dry mass

- Due to the higher I_{sp} and density of LMP-103S additional Δv can be gained for the same spacecraft mass
 - For e.g. 350 kg overall mass the Δv gain is 70 m/s (605 vs. 675 m/s)



Exemplary results

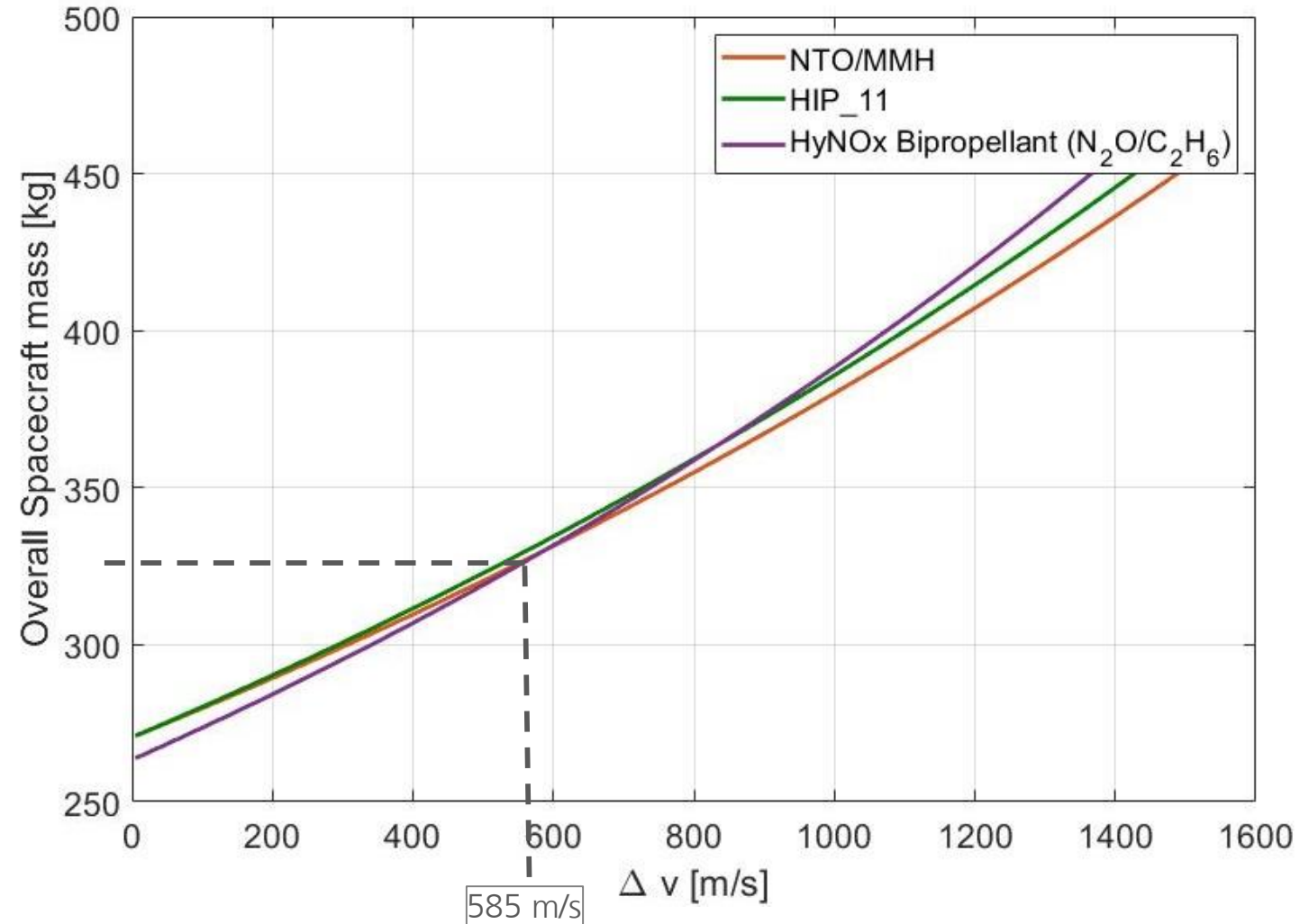
NTO/MMH		
I_{sp}	ϵ	Eff. %
320	330	100

HIP_11		
I_{sp}	ϵ	Eff. %
316	330	96

HyNOx		
I_{sp}	ϵ	Eff. %
314	330	96

Comparison of conventional and green mono-propellant systems for 250 kg spacecraft dry mass

- Up to a Δv of 585 m/s HyNOx beneficial due to lower system mass – no external pressurization needed
- Above Δv of 585 m/s higher Δv available with conventional NTO/MMH
- HIP_11 as hypergolic green propellant is suitable for higher Δv requirements, despite slightly lower performance than conventional NTO/MMH



Exemplary results

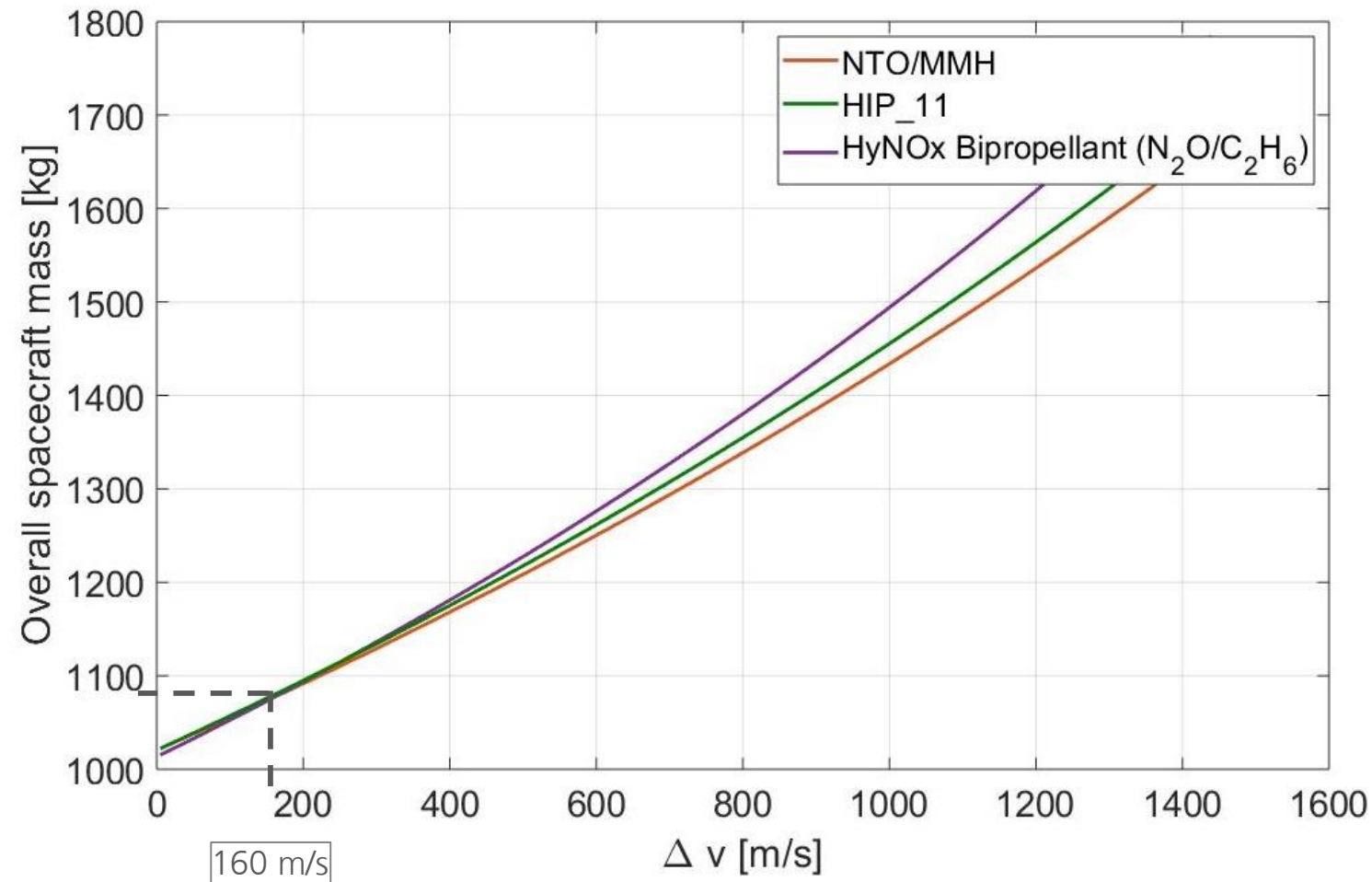
NTO/MMH		
I_{sp}	ϵ	Eff. %
320	330	100

HIP_11		
I_{sp}	ϵ	Eff. %
316	330	96

HyNOx		
I_{sp}	ϵ	Eff. %
314	330	96

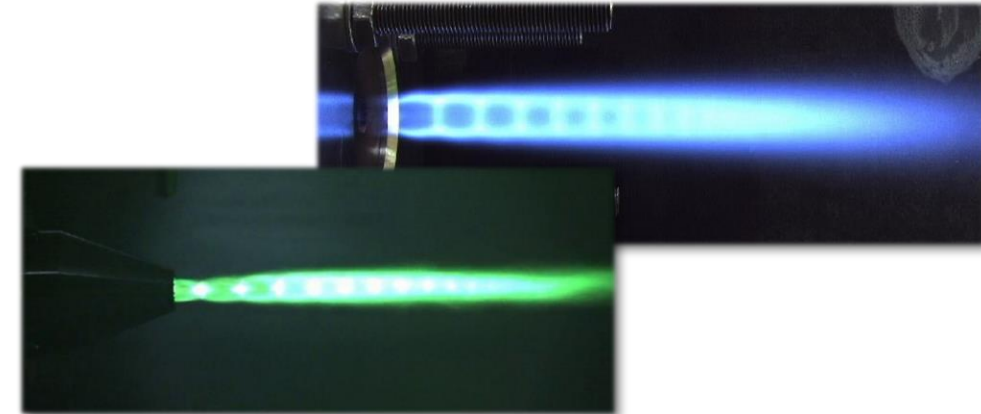
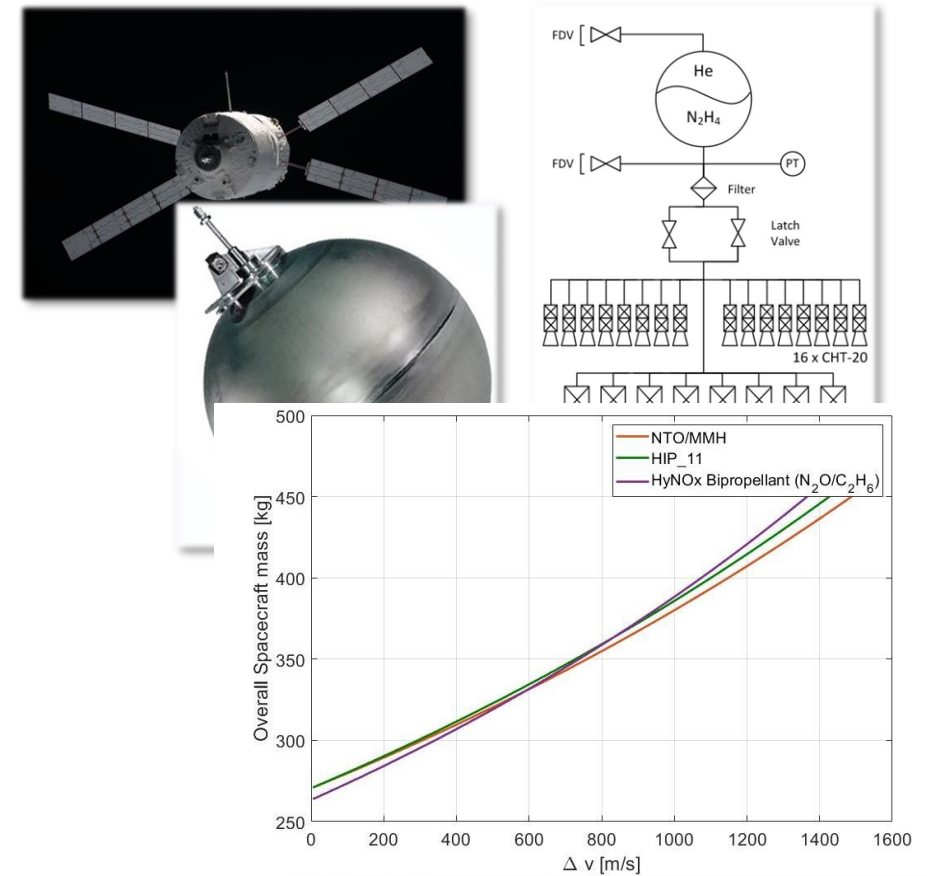
Comparison of conventional and green mono-propellant systems for 1000 kg spacecraft dry mass

- Up to a Δv of 160 m/s HyNOx beneficial due to lower system mass – no external pressurization needed
- Due to lower I_{sp} of HyNOx, lower density and higher tank pressures above 160 m/s HIP 11 or NTO/MMH is advantageous
- HIP_11 as hypergolic green propellant is suitable for higher Δv requirements, despite slightly lower performance than conventional NTO/MMH

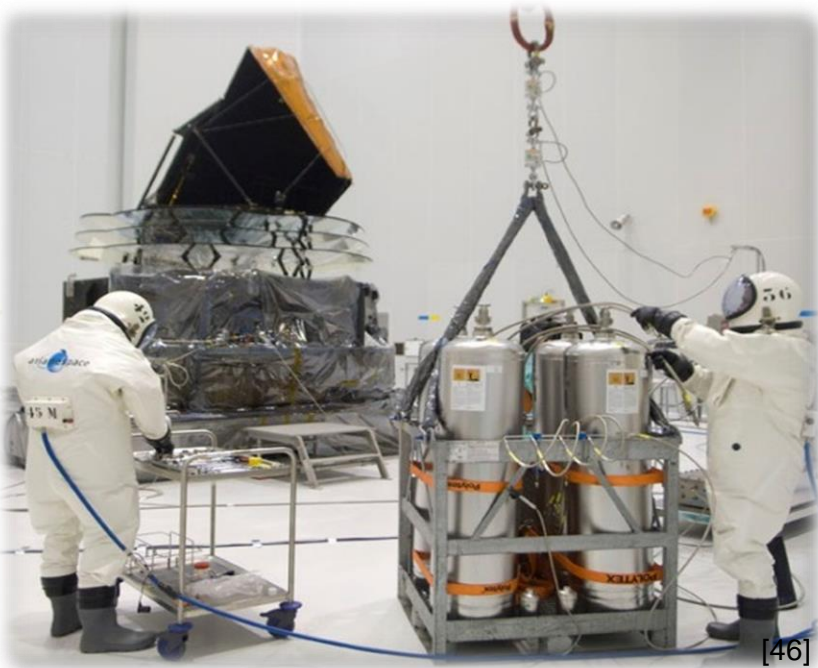


Summary

- Basic comparison tool for different conventional and green propellants developed
- Tool takes spacecraft mass, propulsion system mass, tank masses, propellant, pressurant and thruster masses into account
- A specific propellant can be selected or a generic propellant can be defined
- I_{sp} efficiency, number of tanks (propellant, pressurant), number and size of thrusters can be adjusted
- Green propellants can offer Δv or spacecraft mass advantages compared to conventional propellants, even for lower I_{sp} and/or density
- Tool will be optimized and extended based on available literature data



Thank you for your attention!



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